

A technical report on the:

Implementation and test results of a Beam Current Monitor  
prototype with a Bergoz ACCT

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## 1. INTRODUCTION

The ESS Linac will include in total about 20 Beam Current Monitors (BCMs). These devices are primarily used to measure the beam current and charge, but they will also provide input for the MPS (Machine Protection System) and may also be used for the synchronization of the target wheel to the beam arrival time [1].

It is planned to install most of the BCMS in the low energy end of the Linac (i.e. from the source to the DTL) where there are fewer BLMs (Beam Loss Monitors). In addition to the absolute current measurement, these BCMS will be used to measure the differential beam current (i.e. current difference between two subsequent BCMS) and act on the BIS (Beam Interlock System) if beam losses exceed certain thresholds.

It is planned to use commercial ACCTs (AC Current Transformers) for most of the BCMS. These devices can be used to measure the pulse profile with a measurement rise/fall time of a few hundred ns. In addition to the ACCTs, it is planned to use a few FCTs (Fast Current Transformers) wherever shorter response times are required. The FCT has a bandwidth in the order of a few GHz and can be used, for example, to measure the performance of the MEBT (Medium Energy Beam Transport) choppers with a very short pulse rise/fall time.

## 2. ACCT OPERATING PRINCIPLE

The ACCT is basically a high permeability toroid core with about 10-100 winding turns. The ACCT is mounted on the beam pipe at a location where the beam current has to be measured. The beam goes through the ACCT and generates a voltage across the windings (similar to a one-turn primary winding). This voltage basically has the same profile as the beam pulse, but it does not include the very fast beam variations due to its limited bandwidth. For example, one cannot normally see the individual bunches, but just the envelope of the beam current. Also, there will be a droop of a few % per ms during the pulse flat top. This is because the ACCT lower cut-off frequency normally goes down to a few Hz but does not include 0 Hz. Therefore the ACCT cannot measure DC currents.

The output voltage of the ACCT is then transferred by some cables to the analogue ACCT electronics, where the signal is filtered and conditioned. This electronics is normally supplied by the toroid manufacturer and it is installed out of tunnel to minimize the risk of damage due to excessive radiation from the beam. The output signal of the electronics can then be seen on an oscilloscope or a voltmeter (in case of CW beams).

At ESS, it is planned to integrate the BCMS into the ICS (Integrated Control System). Therefore, the analogue signal from the ACCT electronics has to be digitized, processed and sent to the user interface via the control network as described in the following sections.

### 3. THE BERGOZ ACCT

Figure 1 shows a picture of the Bergoz ACCT and its associated electronics, which were used for the tests.

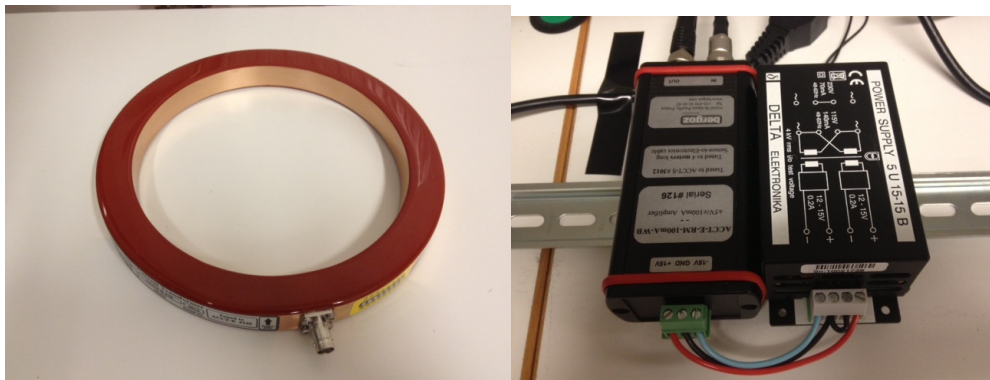


Fig. 1: the Bergoz ACCT (left) and its electronics (right)

Table 1 summarizes the main technical specifications of the ACCT [2]:

Table 1: Main specifications of the Bergoz ACCT

Input current	$\pm 100$	mA
Connectors	Sensor: BNO (bipolar BNC)	
	Electronics input: BNO	
	Electronics output: BNC	
Output full scale	$\pm 5$	V
Lower -3 dB cutoff freq.	3	Hz
Upper -3 dB cutoff freq.	1	MHz
Droop	$< 2$	%/ms
Slew rate	2	V/ $\mu$ s
Output offset	0.5	mV (MAX)
Noise at 100 mA full scale	$< 20$	$\mu$ A (RMS)
Power Supply	$\pm 5, 100$	V, mA

#### 4. CONTROL BOX AND DATA ACQUISITION ELECTRONICS

A demo MTCA.4 control box (see Figure 2) was used for the ACCT tests. The control box consists of the following items [3]:

- 019 chassis from Schroff (including a power supply unit)
- NAT MCH
- GEN2 CPU unit from CONCURRENT TECHNOLOGIES
- SIS8300 digitizer card from Struck
- SIS8900 RTM from Struck

In order to be able to properly measure the ACCT signal, channel 5 and channel 6 of the data acquisition electronics were configured for DC coupling (by default, all the 10 input channels were AC coupled). This was done by de-soldering and soldering some 0 Ohm resistor bridges on both the SIS8300 and SIS8900 cards.

The clock source of the SIS8300 card was set to 'internal' with a clock frequency of 88 MHz. The frequency was chosen to be equal to the planned data acquisition clock from the MRF (Micro Research Finland) timing system.

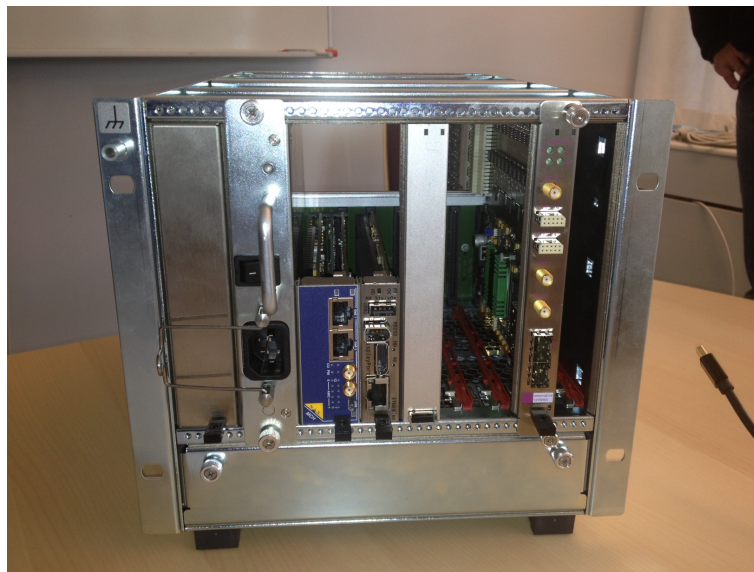


Fig. 2: picture of the demo MTCA.4 control box and the hosted modules

#### 5. ACCT TEST SETUP

Figure 3 shows a picture of the ACCT test setup. The oscilloscope, which was used for these tests, has a waveform generator port. This port was primarily used to generate a 2.86 ms rectangular pulse with an amplitude of 3.6 V across a 146 Ohm resistor, thus generating a current pulse of 24 mA for the ACCT. Later on, the oscilloscope was replaced with a waveform generator generating the rectangular pulse for the ACCT. The output signal of the ACCT, after being filtered and conditioned by the Bergoz electronics was fed into the fifth channel of the RTM and then sampled and digitized by the Struck SIS8300 card hosted by the MTCA.4 system. The control box was connected to the ESS EPICS control system through its drivers and an EPICS application, thus providing the user with a possibility to

control and monitor the whole setup from a remote console in the preliminary ESS Control Room.

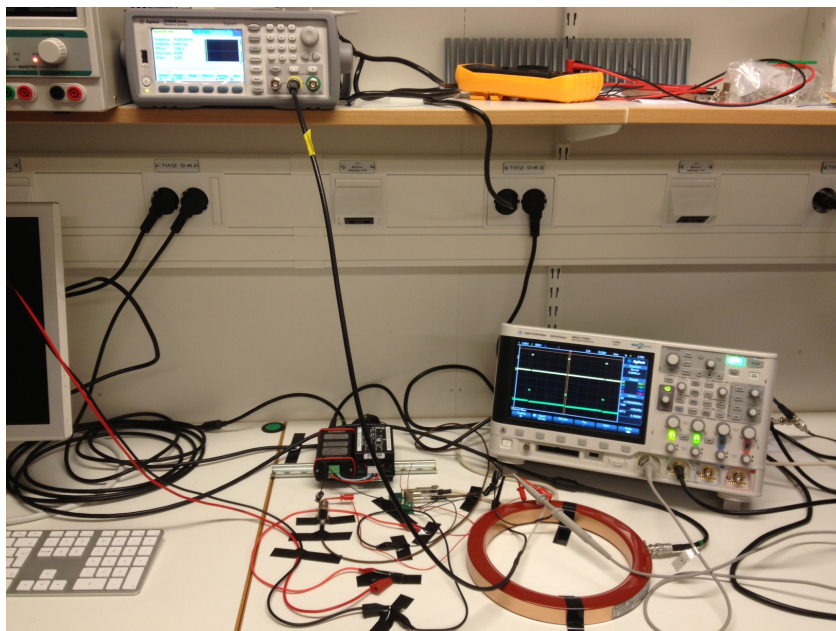


Fig. 3: picture of the ACCT test setup

For these tests, although the MRF timing system was available and ready, due to the lack of a current pulse generator, the control box could not be triggered from the timing system. For that reason, the pulsed voltage generated by the oscilloscope was also used to trigger the control box, thus identifying the start and end of the simulated beam pulse. A small trigger board (Fig. 4), was used to adapt the trigger signal to input of the control box.

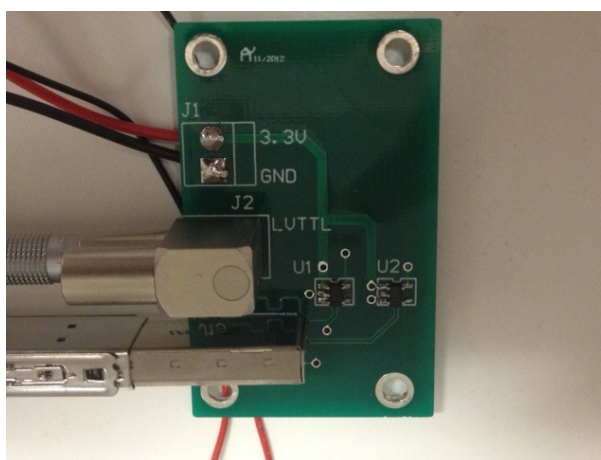


Fig. 4: picture of the trigger board for TTL – LVDS conversion; the board was designed by Andrew Young from SLAC and assembled at ESS



## 6. CONTROL SOFTWARE

The software for the integration of the ACCT into the EPICS control system was mainly provided by Cosylab. This consists of a user-space driver, an EPICS application and a GUI (Graphical User Interface). The kernel driver of the SIS8300 card was supplied by Struck.

Figure 5 shows a snapshot of the GUI with a graphical view of the pulsed current and its specifications, being: average current, charge per pulse, cumulative charge and mA-equivalent of the signal level before the pulse (referred to as "background" signal). The update rate of the GUI is 2 Hz approximately.

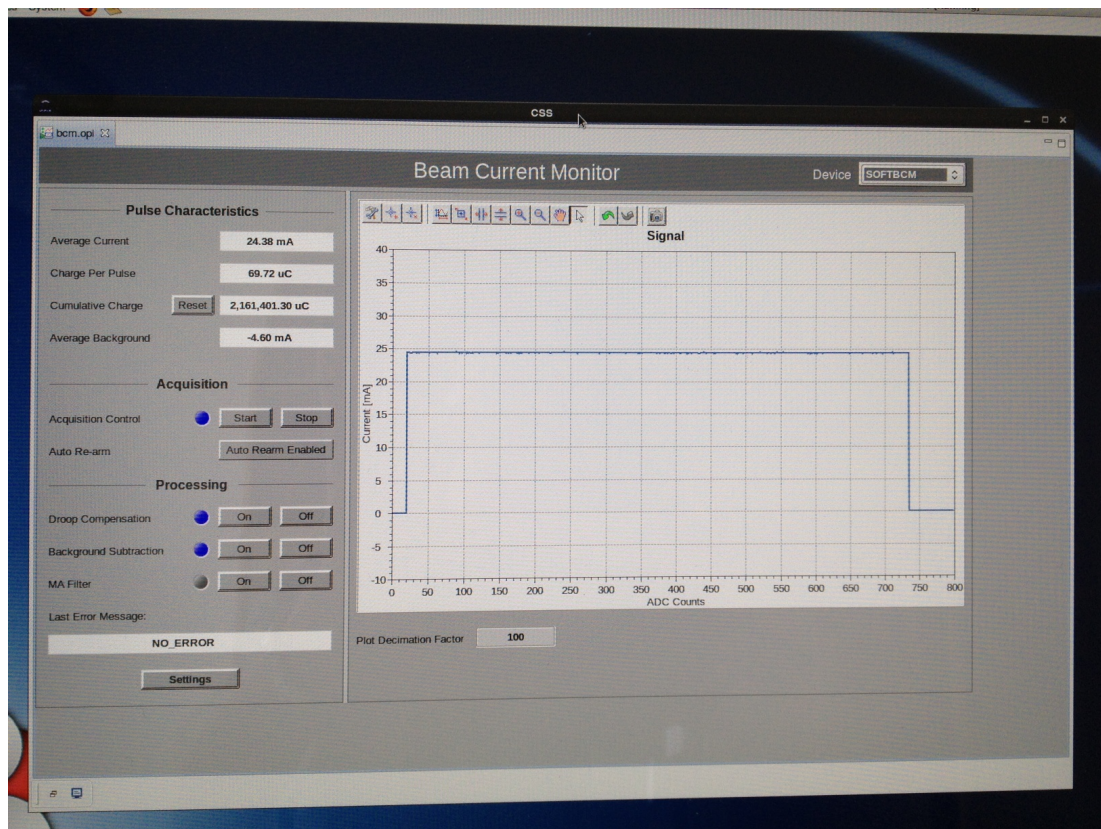


Fig. 5: Snapshot of the ACCT GUI showing the current pulse specifications and profile

As the ACCT cannot measure DC currents and due to the ACCT droop, the background signal is normally negative while the actual current before the pulse is zero. The background signal is then subtracted from the sampled signal so that the monitored value on the GUI reflects a correct measurement.

A button was provided on the GUI to enable/disable droop compensation. When enabled, the instantaneous current over the pulse is multiplied by a factor, which linearly increases with time from the start of the pulse, thus compensating the ACCT droop. The user should therefore insert the ACCT droop factor in the "Settings" window. When the droop compensation is enabled, the pulse becomes very close to DC during the flat-top period of the rectangular pulse.

Other options provided on the GUI include a moving window averaging (with adjustable length) for the pulse profile and the average current measurement, zoom in/out and save options for the graph and a manual/auto re-arm mechanism for the data acquisition.

## **7. TEST RESULTS BEFORE CONNECTION TO THE CONTROL BOX**

The test results of the ACCT before its connection to the Control Box were reported in [4]. The results were promising and in all cases consistent with the ACCT datasheet [2].

## **8. TEST RESULTS AFTER CONNECTION TO THE CONTROL BOX**

The ACCT system was continuously put into operation during a period of one month approximately. The read-back signals were checked from time to time on the GUI with the aim of identifying any malfunctioning of the ACCT hardware, the control box or the control software. The system worked as expected and no problems were seen during this period.

## **9. FUTURE WORKS/IMPROVEMENTS**

With the current version of the GUI, a moving average filter is applied to the pulse waveform to reduce noise. As a result of this, the rising and falling edges of the pulse always are very close to straight lines with a slope depending on the width of the averaging window. While the moving average filter seems to be a good option for the average current measurement (numerical value) its effect on the pulse shape may not be desired, as it does not give any useful information to the end user. The main aim of the pulse waveform is to provide the user with the possibility to check the shape of the pulse, for example the rising and falling edges for any unexpected beam behaviour. For that reason, it is planned to use another filtering method (ex. a low pass FIR filter) for the waveform. The filter bandwidth can then be set so that on one hand the user sees a nearly-real pulse shape (within the measurement bandwidth) and on the other hand reduce noise to a desired level.

Also, it is planned to trigger the Struck SIS8300 using the MRF system (currently, it is triggered with the input signal of the ACCT). Although this is not expected to have any effect on the on-going measurements, it will resemble the final setup more closely; hence it could be useful for identifying and removing any potential problems.

The BCM system will be one of the first beam diagnostic subsystems to be used in the Linac. One of its main functionalities is to measure differential beam currents and act on the BIS (Beam Interlock System) if beam losses are too high. For that purpose, the read-back signal from two or more BCMs have to be compared with each other and appropriate alarm/fault signals have to be sent to the GUI/MPS if the difference exceeds some user-defined thresholds. As the reaction time for the differential current measurement should be in order of a few  $\mu$ s, it cannot be implemented in the control software. Therefore it is planned to transfer that part of the processing to the low-level electronics (i.e. the FPGA). Also, it might



be useful to add some more custom-code to the FPGA firmware; for example a digital low pass filter acting on the acquired samples for noise reduction purposes before sending the samples to the control software. The source code of the FPGA firmware (VHDL) has been provided by the manufacturer. It is planned to first understand the code and later modify it to implement these additional functionalities.

Also, the option of connecting the BCM system to the data logging will be studied. The raw (or slightly processed) ADC data will then be saved in a database and could later on be retrieved upon a user request. This could be a useful option to make a history of the data thus evaluating the long-term behaviour of the BCM system.

## **10. REFERENCES**

[1] ESS Technical Design Report, 13 Nov. 2012

[2] Bergoz Instrumentation, AC Current Transformer User's Manual

[3] H. Hassanzadegan, A technical report on the EPICS integration and preliminary results of the demo BPM MTCA.4 system, ESS internal report, 9 Nov. 2012

[4] H. Hassanzadegan, Test results with the Prototype Bergoz ACCT, ESS Internal Report, 14 Dec. 2012

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